

# Evaluation Method of Vehicle Steering Characteristics under Straight-Driving with Disturbance

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**KEY WORDS:** Vehicle Dynamics, Human Engineering, Driver Model, Evaluation Technology, Steering System

The authors have previously proposed a driver model based handling quality evaluation method for lane change maneuvers using the identified driver parameter  $\tau_L$  as an unified measure for the evaluation (“Lane change  $\tau_L$ ”). Based on the above previous method, in this study, the handling quality evaluation available for the vehicle motion due to corrective steering during a straight line driving with disturbance has been proposed (“Disturbance  $\tau_L$ ”).

The block diagram of the driver-vehicle system during straight running is shown in Fig.1. The steering angle of the driver model  $\delta_h$  is described as

$$\delta_h = -\frac{h}{1 + \tau_L s} (1 + \tau_h s)$$

A difference between measured steering angle  $\delta_h^*$  and  $\delta_h$  is

$$\delta_h^* - \delta_h = \delta_h^* + \frac{h}{1 + \tau_L s} (1 + \tau_h s)$$

So, a following error  $\varepsilon$  is defined:

$$\varepsilon = (1 + \tau_L s)(\delta_h^* - \delta_h) = (1 + \tau_L s)\delta_h^* + h(1 + \tau_h s)y$$

In order to find driver parameter  $h, \tau_L, \tau_h$  to make the difference between  $\delta_h^*$  and  $\delta_h$  small as much as possible, the following criterion function is defined:

$$J = \int_0^T \varepsilon^2 dt = \int_0^T \left[ (1 + \tau_L s)\delta_h^* + hy + h\tau_h \frac{dy}{dt} \right]^2 dt$$

It is possible for us to find the parameters  $h, \tau_L, \tau_h$  which minimize  $J$ . The parameters to be found are called here the identified parameters and, as is the same in the previous method, the identified parameter  $\tau_L$  is regarded as the measure of the handling quality evaluation. Larger the value of  $\tau_L$ , the higher the vehicle handling quality is. Using a driving simulator, the time histories,  $\delta_h^*$  and  $y$ , needed for the identification are measured in this study during the driver-vehicle running on the driving course with the pulse type of lateral force and yaw moment disturbances as shown in Fig.2.

The results of the evaluation are shown in Fig.3 by the identified  $\tau_L$  for the vehicles of both good handling response and deteriorated one. The same aspects of the effect of the vehicle response characteristics on the handling quality,  $\tau_L$ , are obtained by the evaluation methods of “Disturbance  $\tau_L$ ” as well as “Lane change  $\tau_L$ ”. Further-more, the three cases of steering-torque and steering-angle characteristics are provided as shown in Fig.4, and the effects of the width of steering hysteresis on the vehicle handling quality of the vehicles of both standard response characteristics and deteriorated ones are investigated. The results are shown by the normalized  $\tau_L$  obtained by “Disturbance  $\tau_L$ ” method in Fig.5. It has been shown that for the standard response characteristic vehicle, relatively large hysteresis loop characteristics of the steering system is better from the handling quality view points on the other hand, for the vehicle of deteriorated response characteristics, the hysteresis width seems better to be a little bit reduced from the handling quality points of view. This view coincides with a result of the previous study obtained by one of the authors of this study.

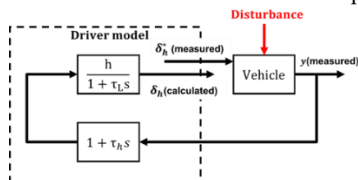


Fig.1 Block diagram of driver-vehicle system during straight running with disturbance

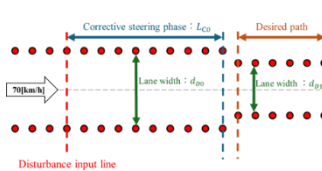


Fig.2 Driving course for evaluation tests

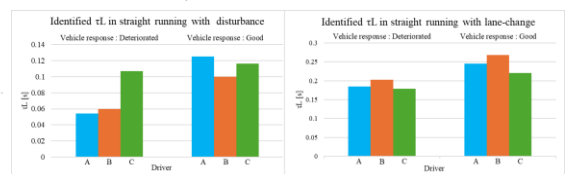


Fig.3 Identified  $\tau_L$  in evaluation tests

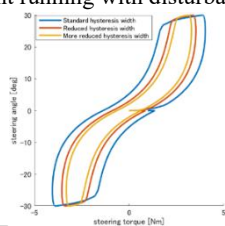


Fig.4 Hysteresis loops of steering angle to steering torque

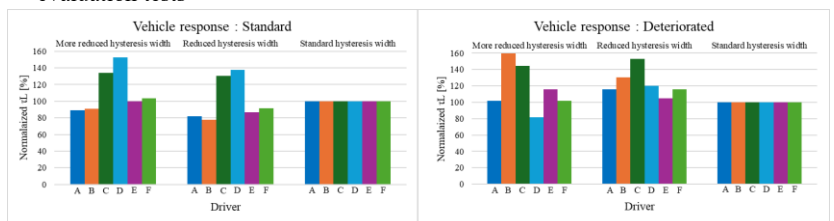


Fig.5 Normalized  $\tau_L$  in evaluation tests of the effects of hysteresis width